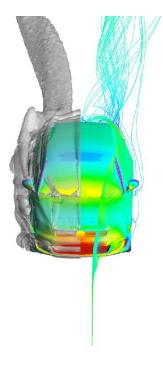


# MK7 Golf R

# Performance of Verus Engineering Diffuser and Dive Planes



Author: P. Lucas Release Date: 2017/09/22 Approvals: E. Hazen

**Document Revisions** 

Rev	Date	Author	Description
01	2017/09/22	P. Lucas	Issued for Release



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- 1. Executive Summary
  - Increased downforce
  - Neutral with drag
  - Improved overall aerodynamic efficiency
  - Package is rear diffuser and dive planes

All work was done using ANSYS software: geometry preparation was completed using SpaceClaim, meshing was done with Fluent Meshing, setup and solution was computed on ANSYS Fluent, and post-processing was completed in CFD-Post.

# 1.1. Coefficient Deltas

ΔCd	ΔCΙ	Aerodynamic Balance (Fr/Rr)
+0.00	-0.502	56/44
Figure 1 1 1. Coofficient Deltas		

Figure 1.1.1: Coefficient Deltas

# **1.2.** Aerodynamic Forces

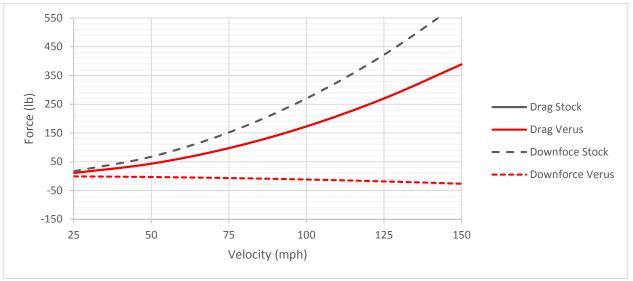


Figure 1.2.1: Aerodynamic Forces at Speed

Aerodynamic forces change with the square of velocity. This is why a single downforce number cannot be given unless it is at a specific speed. Most OEM road vehicles create lift from the factory. With the rear diffuser and dive planes, downforce is increased quite substantially. This downforce added removed all the lift the Golf R created from factory. An increase in overall aerodynamic efficiency will lead to faster track times around the track.



#### 1.3. Summary Plots

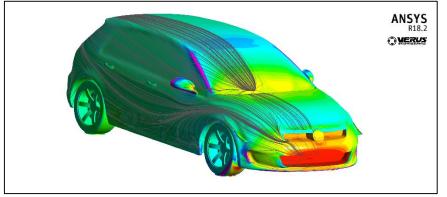


Figure 1.3.1: Cp Plot with Surface Streamlines of the Golf R

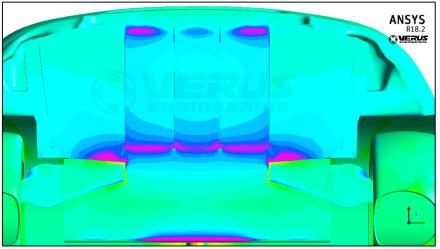
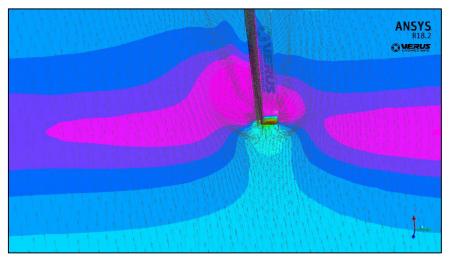


Figure 1.3.2: Cp Plot of the Diffuser



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Figure 1.3.3: Cp Plot on Rear Diffuser – Zoomed-In View by Strake

Figures 1.3.1, 1.3.2, and 1.3.3, we have a Cp Plot (Coefficient of Pressure) which quickly and easily shows us the pressure on different surfaces of the car including the Verus Engineering components. Low pressure is wanted on the bottom side of the components like the rear diffuser and dive planes. Figure 1.3.2 and 1.3.3 specifically shows the strong low pressure on the underside of the diffuser.

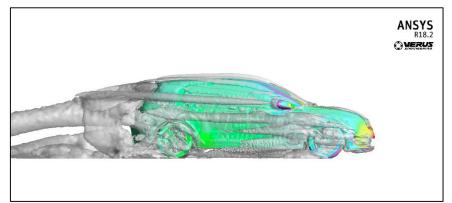


Figure 1.3.4: Q-Criterion Side

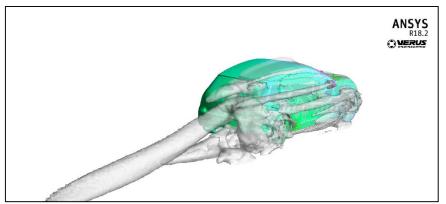


Figure 1.3.5: Q-Criterion Rear



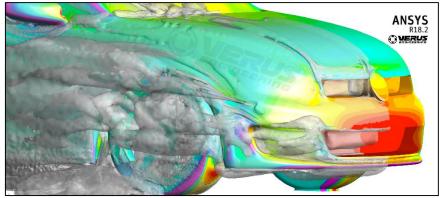


Figure 1.3.6: Q-Criterion Close Up on Front

In Figures 1.3.4, 1.3.5, and 1.3.6 show Q-Criterion plots which highlight areas of vorticity. Q-Criterion helps locate vortices and allows us to direct vortices to locations where they can be utilized efficiently and positively. Notice the strong vortices forming from the dive plane, rear of car, and side mirrors. This strong vortex on the dive plane is one of the reasons flow can stay attached at such a high angle of attack.

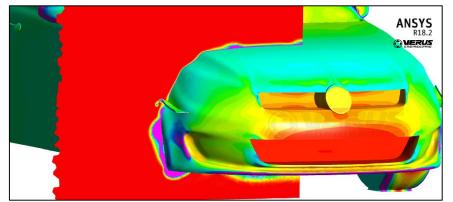


Figure 1.3.7: CpT Plot around Dive Plane



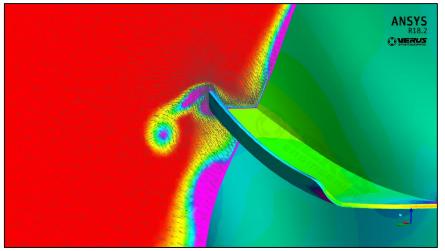


Figure 1.3.8: CpT Plot Close Up at Dive Plane

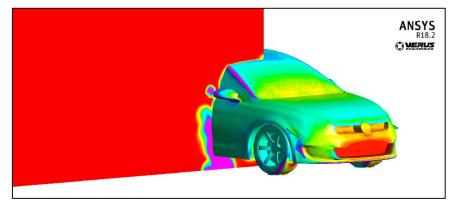


Figure 1.3.9: CpT Plot Just Behind the Side Mirror

In Figures 1.3.7, 1.3.8, and 1.3.9, we have a CpT (coefficient of total pressure) plot. CpT locates free stream flow, red signifying free stream flow. The other colors represent disruptions in this flow. CpT plots also depict vortices. In Figure 1.3.7 and 1.3.8, notice the vortex forming on the dive plane. These vortices help keep flow attached at high angles of attack. The vortex coming off the side mirror can be seen in Figure 1.3.9. This vortex is caused by the pressure gradient between the top and bottom surface.



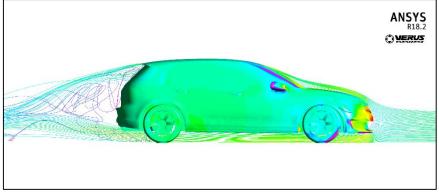


Figure 1.3.10: Side Streamlines

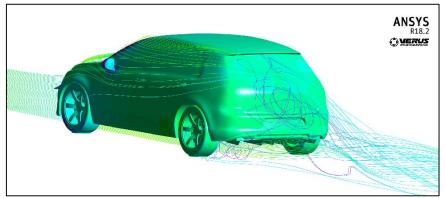


Figure 1.3.11: Rear ISO Streamlines

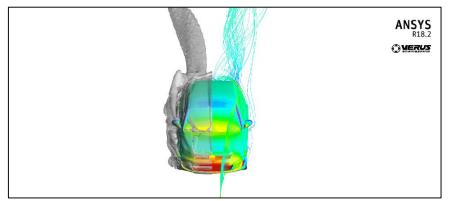


Figure 1.3.12: Front Streamlines

Figures 1.3.10, 1.3.11, and 1.3.12 show streamlines over cars body. Streamlines are another tool used to locate vortices and visualize the general flow field around the vehicle. Streamlines are used by us to verify devices are utilized and directing airflow correctly. Figure 1.3.10 specifically shows the diffuser working with how the streamlines flow off the rear.



#### 2. ASSUMPTIONS

#### 2.1. Geometry

In many automotive analysis cases, simplification of the geometry is required. Analyzing a fully detailed automotive case is not necessary, and much of the critical information we are after could get lost in the plethora of data. The proper approach to the analysis is to setup a simplified physical model. [1] In the automotive case, we isolate particular aspects of the system to capture and ensure we can set proper boundary conditions. In these cases, we are interested in the overall flow field around the Mk7 golf R and how the Verus Engineering Diffuser and Dive Planes improve the aerodynamic efficiency. The simplifications made were as follows:

- Simplified wheels and brakes
- Simplified underbody
- Simplified suspension
- Simplified door handles
- Solid grill surface
- Removed all car panel gaps

#### 2.2. Setup

Some physical effects are removed from the analysis because it is not necessary for these cases. We are looking at the overall flow field around the Mk7 Golf R, some of the physical models are left out. The simplifications made were as follows:

- No radiator flow
- No under hood flow
- No engine intake
- No exhaust flow

#### 3. MESH QUALITY AND METRICS

#### 3.1. Metrics

A proper mesh is essential for a CFD analysis. With CFD, a poor mesh causes the simulation to not converge. Without convergence, the solution will never be reached, and without a good mesh, it is irresponsible to expect accurate results. Here at Verus Engineering we use two main metrics to evaluate mesh quality: skewness and orthogonal quality.

Orthogonal Quality (OQ)	On face	
Derived directly from	A <sub>1</sub>	
Fluent solver discretization		
• For a cell it is the minimum of: $\frac{A \cdots f_{i}}{ \overrightarrow{A}_{i}    \overrightarrow{f}_{i} } = \frac{A \cdots c_{i}}{ \overrightarrow{A}_{i}    \overrightarrow{\alpha}_{i} }$	A <sub>3</sub>	2
computed for each face <i>i</i> $A_i \cdot e_i$		
For the face it is computed as the minimum of $\vec{ \vec{A_i}  \vec{e_i} }$ computed	for each edge <i>I</i>	
Where Ai is the face normal vector and fi is a vector from the centroid of the cell to the centroid of that face, and ci is a vector from the centroid of the cell to		
the centroid of the adjacent cell, where <i>ei</i> is the vector from the centroid of the face to the centroid of the edge	0 Worst	1 Perfect
At boundaries and internal walls <i>ci</i> is ignored in the computations of		
At soundaries and internal wais or signored in the computations of		ANSYS

Figure 3.1.1: Orthogonal Quality Metrics





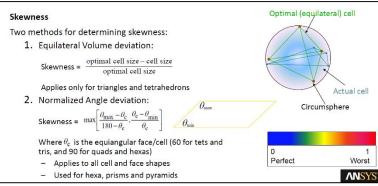


Figure 3.1.2: Skewness Quality Metrics

#### 3.2. Quality

Low orthogonal quality and high skewness values are not recommended for a quality mesh. In general, we always want an orthogonal quality greater than 0.1 and skewness below 0.95. The value may differ depending on the physics and location of the cell.

Orthogonal	Quality	mesh	metrics	spectrum
orthogonal	quanty	THC5H	incures.	Spectrum

Unacceptable	Bad	Acceptable	Good	Very good	Excellent
0-0.001	0.001-0.14	0.15-0.20	0.20-0.69	0.70-0.95	0.95-1.00

Figure 3.2.1: Orthogonal Quality Metrics

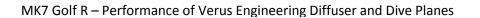
Skewness mesh metrics spectrum					
Excellent	Very good	Good	Acceptable	Bad	Unacceptable
0-0.25	0.25-0.50	0.50-0.80	0.80-0.94	0.95-0.97	0.98-1.00

Figure 3.2.2: Skewness Quality Metrics

#### 3.3. Types of Mesh

There are two main types of meshes, or grids: structured and unstructured. Structured grids generally have better convergence and higher accuracy with a more simple flow field. Unstructured grids are more commonly used for Verus Engineering applications since geometry and flow fields are complex.





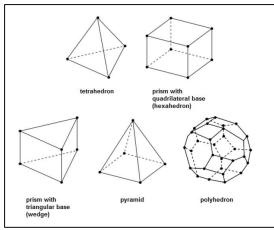


Figure 3.3.1: Volume Cell Shapes

An unstructured mesh using prism layer for boundary layer resolution and polyhedron for the volume was utilized in this case. An advantage that polyhedral meshes have shown relative to tetrahedral or hybrid meshes is the lower overall cell count, almost 3-5 times lower than the original cell count. [2] Also since cell count is lower per the equal refinement, convergence will generally be faster.

# 3.4. Mesh Quality

All meshing is completed using Fluent Meshing. Fluent Meshing allows Verus Engineering to setup a quality grid for proper solution and convergence.

Skewness was not above 0.76. This is in the acceptable zone for the minimum orthogonal quality. The majority of the mesh is in the very good to excellent range. The volume mesh had a cell count just over 16 million.

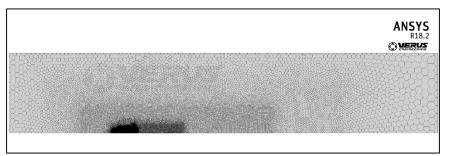


Figure 3.4.1: Mesh Domain



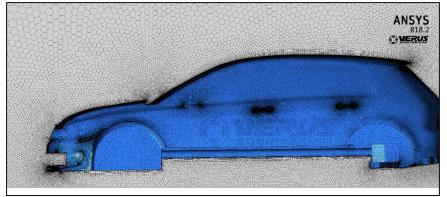


Figure 3.4.2: Mesh at Symmetry Plane

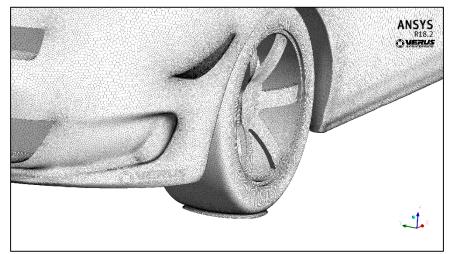


Figure 3.4.3: Surface Mesh

# 4. ANALYSIS SETUP

#### 4.1. General

ANSYS Fluent – a finite volume discretization scheme - is used for solving all of Verus Engineering external aerodynamics cases. The solver used is the semi-implicit method for pressure-linked equations, SIMPLE. [3] These cases were solved using the steady-state method which ignores the higher order terms dealing with time.

# 4.2. Boundary Conditions

Boundary conditions are used to define the computational problem. Without boundaries, nothing can be solved, and proper boundary conditions are a must for an accurate analysis. A full understanding of the physics of the problem is a must. CFD only emulates the condition of the road and track, it does not reproduce it. Simulations inherently deviate from reality and it is often hard to quantify all the sources of error. The cases were solved using symmetry on the XZ Plane. This decreased the mesh quantity by cutting the computational domain in half, thus decreases the simulation time to convergence. Using symmetry on the XZ Plane is standard in the industry unless you are modeling yaw. The case is modeled using a virtual wind tunnel **Confidential: Property of Verus Engineering. Not for Distribution outside intended recipient list**.



which is discretized and used as the fluid volume. The air then flows over the stationary car in the boundary. The ground and wind tunnel walls have the shear equal to zero to not have boundary layer growth which simulates the rolling road condition to have a proper flow regime. The wheels are setup as a rotational moving wall boundary.

Inlet	Inlet Condition	45 m/s	
Outlet	Pressure Outlet Condition	0 Pa (Gauge)	
Symmetry Plane	Symmetry	N/A	
Ground	Wall Condition	Shear = 0	
Wind Tunnel Walls	Symmetry	N/A	
Car	Wall Condition	No Slip Shear	
Wheels	Wall Condition	141 rad/s	

Figure 4.2.1: Boundary Conditions

#### 4.3. Turbulence Modeling

The majority of fluid flows in engineering cases are turbulent. Because of this, a proper turbulence model is needed for proper results and flow regimes. The k-omega SST turbulence model was used in these cases. The k-omega is great for solving flows in the viscous sublayer (boundary layer). The SST allows the model to solve free-stream area where the normal k-omega was too sensitive to free-stream turbulences. [4]

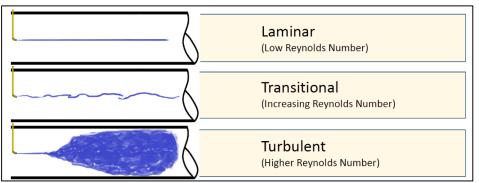


Figure 4.3.1: Flow Classifications

# 5. ERRORS IN SIMULATION

# 5.1. Physical Model

Some of the errors in the physical model were discussed in Geometry Assumptions. The substitution of a CAD model from a real physical model is an inevitable source of error. The CAD model only represents part of the physical system, others are either represented with boundary conditions or removed from the analysis.

# 5.2. Discretization Error

Discretization errors are those errors that occur from the representation of the governing flow equations and other physical models as algebraic expressions in a discrete domain of space and



time. As the mesh is refined, the solution should become less sensitive to discretization error. These errors can be analyzed using grid convergence study. [5]

#### 6. <u>CONCLUSION</u>

The goal of the diffuser and dive planes were to work as a package for the Mk7 Golf R to improve aerodynamic performance over stock. The package is designed for the enthusiast who frequent track days and want an effective aerodynamic package that balances the car at speed. Both components were designed to work together as a package.



#### **REFERENCES**

- [1] Zikanov, Oleg. *Essential Computational Fluid Dynamics*. 1<sup>st</sup> Edition. John Wiley & Sons, Inc., 2010.
- [2] ANSYS Fluent Meshing User's Guide, 18.1, April 2017.
- [3] Patankar, Suhas. Numerical Heat Transfer and Fluid Flow. 1<sup>st</sup> Edition. Hemisphere Publishing Corporation, 1980.
- [4] Menter, Florian. Improved Two-Equation k-w Turbulence Models for Aerodynamic Flows. NASA Technical Memorandum, no. 103975 (1992).
- [5] Slater, John. 2008. Uncertainty and Error in CFD Simulations. <u>https://www.grc.nasa.gov/WWW/wind/valid/tutorial/errors.html</u> (Accessed 2016-09-20).